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漂木灾害研究现状及研究展望

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摘 要: 漂木是山地系统中常见的物质组成,在山地系统中发挥着重要的生态功能。随着山地灾害日益加剧,漂木在被山洪、泥石流搬运过程中常造成严重的灾害效应。基于国内外研究成果,文章首先分析了漂木的运动与堆积规律;在此基础上,从漂木堆积导致的侵蚀作用、雍水作用、溃决作用和漂木冲击作用等四个方面总结了漂木的灾害效应,对漂木灾害效应的评估方法以及常见的漂木灾害减灾措施进行了详细梳理。基于山地灾害防灾减灾需求,分析评价了目前研究存在的问题,提出了应加强基于真实情境的漂木运动堆积规律研究,加强大规模山地灾害条件下漂木灾害效应的研究以及漂木灾害治理过程中去除漂木带来的灾害效应的研究。

关键词: 山洪;泥石流;漂木;灾害效应

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漂木是指普遍存在于山地系统中由滑坡崩塌、沟岸侵蚀、火灾、风力作用、自然死亡或人为砍伐等各种因素产生的大量枯倒木。从生态和地貌学而言,其在山地系统中发挥着重要的生态功能,对沟道地形地貌的塑造产生积极的影响,为水生生物提供有效栖息场所,增加生态多样性等^[1-2]。近年来,世界范围内山地灾害暴发越加频繁,滑坡、崩塌、沟岸侵蚀等过程产生大量的漂木源^[3],并在山洪泥石流作用下被搬运,其产生的灾害效应受到越来越多的关注,尤其是在植被较好、人口密度较大、山地灾害频发的地区,威胁附近建构物及人们的生命财产的安全^[4]。例如,1999 年 12 月委内瑞拉特大泥石流^[5]、2005 年 8 月瑞士全国范围内的特大洪灾^[6]、2007 年 9 月斯洛文尼亚 Davča 流域的洪灾^[7]、2011 年 10 月意大利 Magra 流域的洪灾^[8]、2003 年 7 月中国云南德宏泥石流^[9]、2009 年 8 月中国台湾莫拉克台风事件^[10]、2013 年 7 月中国四川汶川草坝乡泥石流(图 1)和七盘沟泥石流等(图 2),漂木广泛存

在于堆积体中。

关于山地灾害中的漂木灾害效应的相关研究才刚起步,资料很少^[8],而以中文文献发表的相关研究成果就更少。本文从灾害效应角度出发,对国内外已有研究进行评述与研究展望,主要包括以下几方面:(1)漂木的运动与堆积规律;(2)漂木的灾害效应;(3)漂木灾害评估与减灾措施,为开展山地灾害过程中漂木灾害效应的研究提供参考。

1 漂木运动与堆积规律

漂木的运动与堆积规律是正确认识与理解漂木致灾机理的基础,也是漂木灾害评估与防灾减灾的前提,对其研究多采用实地调查统计、实验模拟和数值模拟等方法进行研究。早期实地调查与大量实验研究表明漂木的启动方式主要有滑动启动与滚动启动两种,漂木长轴与水流方向的初始夹角不同将导致不同的启动方式,当漂木长轴垂直于水流方

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图1 2013年四川汶川县草坡乡泥石流:(a)漂木堵塞于楼房内;(b)漂木堆积于房屋前

Fig. 1 Caopo debris flow of 2013 in Wenchuan County, Sichuan Province

(a) Woody debris deposited inside a house; (b) Woody debris deposited in front of a house



图2 2013年四川汶川县七盘沟泥石流:(a)漂木散布于沟道堆积物表面;(b)沟道中漂木形成的堵塞体拦截泥沙

Fig. 2 Qipan debris flow of 2013 in Wenchuan County, Sichuan Province

(a) Woody debris distribute on the surface of debris flow deposition; (b) Woody debris accumulation intercepts sediment in a channel

向时将滚动启动,而顺水流方向则滑动启动,除此之外,影响漂木启动的因素还有漂木量、漂木直径、漂木形态等^[11-12]。长漂木比短漂木运动的距离更长,在宽度大的沟道里漂木运动距离更长^[13-14];大量漂木在河道里运动可呈现堵塞、半堵塞及不堵塞三种形态^[15]。漂木的堆积多发生在沟岸、浅滩、弯道、障碍物等条件下^[16-17]。概括起来,漂木运动形态、运动距离及堆积分布规律与漂木量、漂木特征、沟道地形地貌特征及水流特征等因素有关。

在这些认识的基础上,描述漂木运动及堆积规律的数值模型逐渐发展起来。Mazzorana等提出了一个计算给定漂木量可能运动路径的2D水力学模型^[18], Ruiz-Villanueva等提出了一个目前为止最为综合的数值计算模型——Iber-Wood 2D模型^[19],该模型可用于反演、推算以及情景模拟^[20]。该模型已被成功用于1997年西班牙Cabrera河洪水事件的反演,反演结果显示的漂木堵塞体分布情况、堆积形态等与事后实地调查结果高度吻合^[21]。

2 漂木灾害效应

2.1 漂木堆积加剧侵蚀作用

漂木堆积于沟道岸边、弯道等处,堆积体周围局部水流速度增大、侵蚀能力增强,从而进一步加剧沟岸的侵蚀,导致沟岸失稳、沟道加宽、弯道加剧等^[22]。漂木堆积于桥墩处则会加剧桥墩处水流对泥沙的侵蚀,从而导致桥墩失稳破坏。早在1956年,Laursen就指出漂木在桥墩处堆积增加了桥墩的等效直径,使水流紊度增大,从而加重对桥墩的侵蚀^[23]。桥墩处有漂木堆积时的侵蚀坑深度可达无漂木堆积时的1.42~3倍^[24]。漂木堆积体的密实度是影响侵蚀效果的主要因素,漂木堆积体的纵向长度、平面分布对桥墩的侵蚀发展也有较大的影响^[23,27]。漂木在桥梁处堆积的主要方式为单个桥墩的堆积以及桥墩间的堵塞,其堵塞概率、堆积形态和规模受到桥梁上游沟道宽度、桥型、水流状态、漂木特征及桥梁净空高度等因素的影响^[28-30]。

2.2 漂木堆积导致雍水效应

漂木堵塞桥涵等过水通道,致使回水淤积、水位升高,从而导致洪水泛滥面积增大、持续时间延长,加重灾害程度^[31];水位升高也导致了水压力的增大,增加了建构物的荷载,严重威胁建构物的安全^[32],我们将此定义为漂木堵塞导致的雍水效应。理论分析和试验研究表明弗洛德数、漂木堵塞体规模及密实度是影响雍水效应的关键参数,雍水程度随着流体弗洛德数、漂木堆积体长度的增大而增大,随着漂木堆积体直径以及堆积体密实度的增大而减小^[33-35];其次,漂木的形态如枝丫、根系等对漂木堆积体雍水效应的影响也不可忽略^[36]。

2.3 漂木堆积体的溃决效应

漂木堆积体的溃决可能会带来类似土石堰塞坝溃决的灾害放大效应。据报道,1978年瑞士某流域的山洪灾害,由于漂木坝的溃决造成了 $3000\text{ m}^3/\text{s}$ 的洪峰流量,将 $25\ 000\text{ m}^3$ 的漂木送进了下游水电站水库,从而导致了水电站大坝排水通道的堵塞,进而水位升高、漫顶溢流,威胁下游水电站建构物的安全^[37]。通过斯洛文尼亚 Davča 流域 2007 年洪水事件的调查发现,沟道多处出现漂木堵塞体溃决现象^[11]。事实上,大规模山洪泥石流灾害事件中关于漂木堆积体溃决造成的洪峰经常被当地居民目睹,但遗憾的是翔实的调查数据仍然十分匮乏^[8]。初步的实验研究表明在顺直变宽沟道中泥石流挟带漂木形成不稳定坝体溃决后的洪峰流量是未形成堵塞体时的 1.2 倍^[38]。因此,关于漂木堆积体溃决导致的灾害效应亟须更加深入细致的研究。

2.4 漂木的冲击作用

运动中的漂木则对建构物具有一定的冲击力。水槽模拟及现场实验研究表明,漂木撞击的偏心程度对冲击力有较大影响,当漂木长轴平行流线方向且垂直撞击建筑物时,造成的冲击力最大;随着建筑物刚度的增大,漂木冲击力越大,而冲击接触面的材料种类本身对最大冲击力的大小没有影响^[39]。傅宗甫等人利用钟摆原理模拟漂木冲击漂木道的过程,采用应变式冲击力传感器直接测定了漂木的冲击力,得出单位体积内单位速度漂木冲击力只与撞击角度有关^[40]。总体而言,在山洪泥石流搬运过程中漂木对建构物的冲击作用不如大块石的冲击力度大,灾害效应不如侵蚀、堵塞作用明显,但由于其细长的形态,容易卡在建筑物的缝隙中,在外力作用下

形成力矩等附加作用从而导致结构的破坏。

3 漂木灾害评估与减灾措施

3.1 漂木灾害评估

鉴于漂木运动规律的复杂性,漂木灾害评估主要从漂木源地识别、漂木量估算以及漂木分布危险性制图等方面展开了较多研究。漂木量的估算是漂木灾害减灾决策的基本参数,早期的漂木量估算模型多基于流域资料结合统计数据,如 Rickenmann 提出的基于流域面积的潜在漂木量估算经验公式^[41], Uchiogi 提出的基于泥沙量和树木覆盖区域面积的两种漂木量估算方法^[42]。随着地理信息系统技术的发展和先进理论的不提出,基于 GIS 技术、模糊决策理论的漂木量估算与分布模型也逐渐发展起来。Petrascheck 等在山洪泥石流灾害评估的基础上,考虑漂木的影响,通过对漂木源的识别以及危险性指标的计算,利用 GIS 得出漂木分布图及危险等级制图^[43];Mazzorana 等在前人研究的基础上,进一步完善了漂木源地识别及危险指标计算方法,针对流域地势地貌的差别划分不同区域以指导流域植被覆盖规划;发展了基于 GIS 及遥感技术的漂木量估算方法^[44]。然而,这些模型还需要进一步完善,同时还需考虑不同时间尺度的漂木量动态评估、漂木分布预测,特别是需要加强野外监测数据的获取以便检验和修正模型的适用性。

综合性的漂木灾害评估模型则更加复杂,Mazzorana 等提出了一个基于专家经验与模糊决策理论的漂木灾害评估模型^[45],该模型包括风险因素识别与筛选、因子水平确定、风险矩阵建立以及连续情景识别等四个步骤,其中风险因素及因子水平的确定是该模型的关键,因素和因子水平太少会导致模型不具代表性,太多则会大大增加矩阵的复杂程度而使其难以操作。因此,在已有山洪、泥石流灾害风险评估模型的基础上以适当形式考虑漂木的影响应是漂木灾害评估的一个发展方向。

3.2 漂木灾害减灾措施

针对漂木的危害,美国、日本及阿尔卑斯地区的国家较早开展了相应的减灾措施研究,其中阿尔卑斯地区如奥地利发展了较为完善的综合防治措施,包括森林保护措施、土壤生物工程措施、结构工程措施、流域整治措施、水利措施及相应的政府管理措

施^[46]。日本也发展了基于工程措施的流域综合治理措施,防止漂木的产生以及捕获已产生的漂木。Commit 等^[8]认为减轻漂木灾害最为有效可行的措施还是在于:(1)减小桥涵等处的堵塞堆积措施,如进行合理设计或采取被动保护措施,目前,针对桥涵多采用漂木导流桩、导流鳍、漂木清除装置等来减少漂木在桥墩、涵洞处的堆积堵塞^[29,47](图3、图4);(2)在沟道关键断面设置漂木拦截措施。在山洪暴发频繁的阿尔卑斯地区,多采用耙齿型格栅坝、V型栅栏、柔性格网等漂木拦挡工程^[46,48-49](图5)。在

山洪泥石流均较频发的日本,一般采用兼具漂木捕获功能和泥沙拦截功能的A字形泥石流流格栅坝、钢管格子坝、缝隙坝等^[49-51](图6)。在中国,对九寨沟风景区泥石流治理中考虑到了漂木的影响,采取了重力式梳齿坝和缝隙坝来拦挡漂木和巨砾^[52-53]。近年来,一些新的漂木拦截措施被提出来,Schmocker 等发明了一种以排导和分离为主的漂木防治工程即侧路拦截措施^[54](图7),该措施主要由侧路支沟、导流堤、漂木约束栅栏等部分组成,修建在河道弯道的凹岸,导流堤高于平均河水位,以保证



图3 桥墩保护装置:(a) 导流桩^[29]; (b) 导流鳍^[47]; (c) 漂木清扫装置^[47]

Fig. 3 Woody debris protection devices for bridge piers

(a) Debris deflector^[29]; (b) Debris fin^[47]; (c) Debris sweeper^[47]



图4 涵洞保护装置:(a) 导流装置^[47]; (b) 固定式拦截栅栏^[47]; (c) 活动式拦截栅栏^[47]

Fig. 4 Woody debris protection devices for culverts

(a) Steel rail debris deflector^[47]; (b) Fixed debris rack^[47]; (c) Moveable debris rack^[47]



图5 阿尔卑斯地区的漂木防治措施:(a) V型桩林^[46]; (b) 倾斜耙齿拦沙坝^[48]; (c) 柔性格网坝^[49]

Fig. 5 Woody debris mitigation measures in European Alps area

(a) Vertical rake with V-shaped outline^[46]; (b) Check dam with inclined rake^[48]; (c) Flexible debris flow barrier^[49]



图6 日本漂木捕获装置:(a) A形格栅坝^[49];(b) 钢管格子坝^[50];(c) 混凝土缝隙坝^[51]

Fig. 6 Woody debris capture structures in Japan

(a) Check dam with A-type of slit^[49];(b) Grid type steel Sabo dam^[50];(c) Concrete-slit sabo dam^[51]

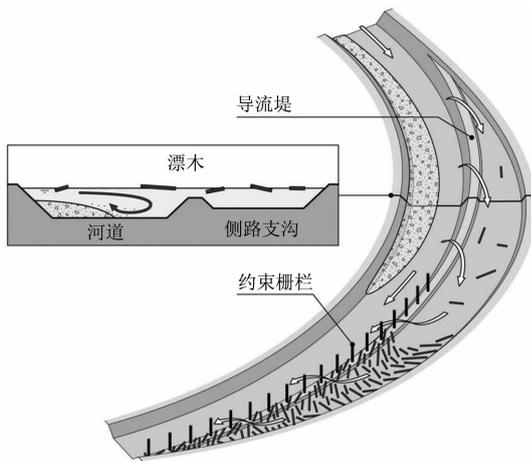


图7 侧路拦截措施示意图^[54]

Fig. 7 Schematic of driftwood bypass retention^[54]

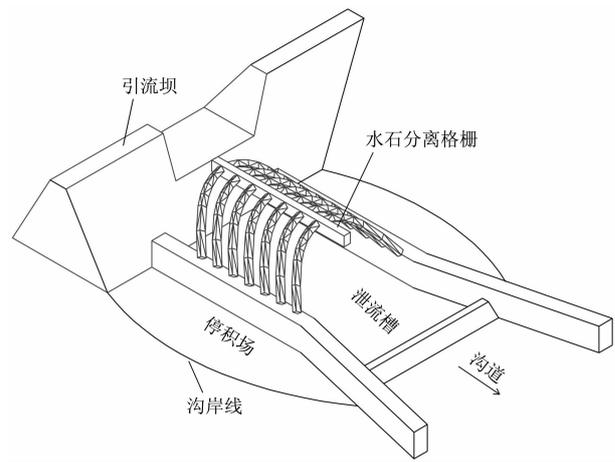


图8 鱼脊型水石分离结构示意图^[55]

Fig. 8 Schematic of herringbone water-sediment separation structure^[55]

侧路支沟只在洪水期间发挥作用。洪水期间水位上升,挟带的漂木在二次流离心力的作用下通过导流堤进入侧路支沟,并被栅栏有效约束起来,从而实现漂木的分离。谢涛等人发明的鱼脊型水石分离结构^[55](图8)经试验证明也具有好的漂木分离效果^[56]。

4 研究展望

4.1 加强基于真实情境的漂木运动堆积规律研究

目前,人们关于漂木的运动与堆积规律已经得到了一些认识。然而,相较泥沙而言,漂木的运动与堆积规律更为复杂,原因在于:(1)理解漂木的运动与堆积规律,其中一个关键的因素是浮力的影响,而浮力又与漂木的种类、干湿状态等因素有关;(2)相比泥沙而言,漂木在形态、尺寸与规模上更加多元化、复杂化。已有的研究多将漂木简化为光滑的圆柱体,但实际情况下漂木可能具有根系、枝丫,形态

极为复杂;其次,漂木的长径比悬殊,其长度方向的尺度往往与沟道宽度相当,易与沟岸、沟道内障碍物产生复杂的作用;(3)漂木量的影响不可忽视,现有研究中多从单根漂木入手建立相关的启动、运动模型,而现实情况下往往是大量漂木相互作用形成聚合体,漂木聚合体的形态特征等将对其运动与堆积规律产生影响,因此与单根漂木在运动堆积规律上将有很大区别;(4)不同性质与规模的流体搬运条件下其运动堆积规律不同。山洪、泥石流历时短、泥沙含量大、侵蚀能力强,在这样的条件下漂木与流体、泥沙、沟道之间的相互作用相较常水流条件下更为复杂。

鉴于上述分析,笔者认为在以后的研究中应逐步加强基于真实情境的运动堆积规律研究,即以自然界中实际发生的事件为原型,提取相关参数,利用模型试验、数值模拟等手段反演运动堆积过程,以促进相关理论的完善,检验研究成果的正确性与准确性。而要做到这一点,其前提是加强对实际灾害事

件的监测,以便获取有效的数据信息,这反过来又促进了对灾害事件预测能力的发展。包括漂木灾害发生条件的识别、漂木源与漂木量估算、数值模拟计算的反演与预测。

4.2 加强大规模山地灾害中漂木灾害效应的研究

虽然,漂木具有一定的灾害效应,大量事件表明似乎只有在大规模(大于50年一遇)的山洪泥石流灾害事件中搬运的大量漂木才能产生较为明显的灾害效应^[3]。然而,并非所有大规模的山洪、泥石流灾害都会搬运大量漂木,根据欧洲几次大的洪水灾害调查表明,其漂木源多来自新鲜树木,也即在山洪、泥石流灾害过程中由滑坡、沟岸侵蚀等产生的新鲜漂木源,而沟道中已存在的枯倒木仅占很小比例^[57]。因此,山洪泥石流灾害中漂木的灾害效应首先受到漂木源供应能力及可搬运能力的限制,这反过来又受到地形地貌、植被覆盖情况、滑坡等过程强度等条件的制约。因此,对漂木源产生条件的界定及漂木量的估算是漂木灾害效应研究的基础。

其次,关于大规模山洪、泥石流灾害条件下的漂木事件的观测资料依然很少。利用先进的科学技术手段技术加大对灾害事件的观测、调查和资料收集,并在此基础上利用观测资料进行相关物理模型实验与数值模拟分析及验证,是今后研究需解决的重要问题。

最后,山地灾害动力过程彼此耦合,若从漂木源形成及搬运的不同动力过程考虑,其可能在滑坡、泥石流等动力过程作用下与沙石形成复合堆积体。复合堆积体的稳定性及溃决模式、特征以及漂木对复合堆积体稳定性的影响是未来需要研究的重要内容,这对山地灾害防灾减灾特别是堰塞坝的稳定性分析与风险评估起到重要的补充与完善作用。

4.3 注重漂木减灾过程中去除漂木的影响

目前,漂木减灾措施很大程度上是通过分离和拦截沟道中的漂木而减少其可能导致的灾害效应。然而,也有研究指出去除河道中的漂木可能造成局部流速增大、加剧沟岸侵蚀、增大洪水泛滥的频率与时间、导致河道萎缩、河流生态系统多样性缺失等问题^[58-60]。Reinfelds等指出通过去除latrobe河道中的漂木可增大河道输运能力67%、平均流速增大两倍左右,而流速的增大加剧了河床的下切,从1925~1994年的统计数据得出,latrobe河下游河床平均下切深度增大了0.25~1.05m不等^[61]。Erskine

等分析了Cann河的历史数据发现,由于大规模的去漂木作用,加之1971年的一次大规模洪水作用,该河在1935~1995之间,河道平均宽度增加了490%,平均流深增加了40%,弯曲度减小了31%,侵蚀输砂量达 $3.3 \times 10^6 \text{ m}^3$,该河由一条流量小、弯曲狭窄、植被覆盖、布满漂木的小河道转变为流量大、含沙量大、宽直裸露、侵蚀活跃的砂床河流^[62]。在此转变过程中,河道中的鱼类急剧减小,生态多样性流失。上述研究表明以后开展的漂木灾害防灾减灾研究中,要从不同时间尺度综合考虑漂木的灾害效应及其对生态环境的影响,特别要考虑到去除漂木的灾害效应,制定科学合理的漂木综合治理与利用措施。

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A Review of the Research on Woody Debris Related Disaster and Its Prospect

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Abstract: Woody debris are quite found in mountain area, and they play significant functions in regulating mountain systems. As geohazards become more predominated in mountains, it may cause serious consequences in the case of transported by debris flow or flash torrents. According to the past researches at home and abroad, in this article it first analyzed the movement and deposition of woody debris, then following by a summary of the hazardous effects from four aspects: erosion effects (especially on bridge piers), backwater effects, dam-break effects of woody debris accumulations and the impact effects of travelling woody debris. Then it concluded the methods of evaluation on woody debris hazards as well as mitigation measures. Based on the needs of mountain geohazard prevention and mitigation, this paper also analyzed the existing insufficiency of current researches, and proposed that much more attentions should be paid on three aspects: woody debris transportation and deposition analysis based on realistic scenario, woody debris related hazards during high-magnitude mountain geohazard events, and the hazard effects related to the removal of woody debris.

Key words: floods; debris flow; woody debris; geohazard